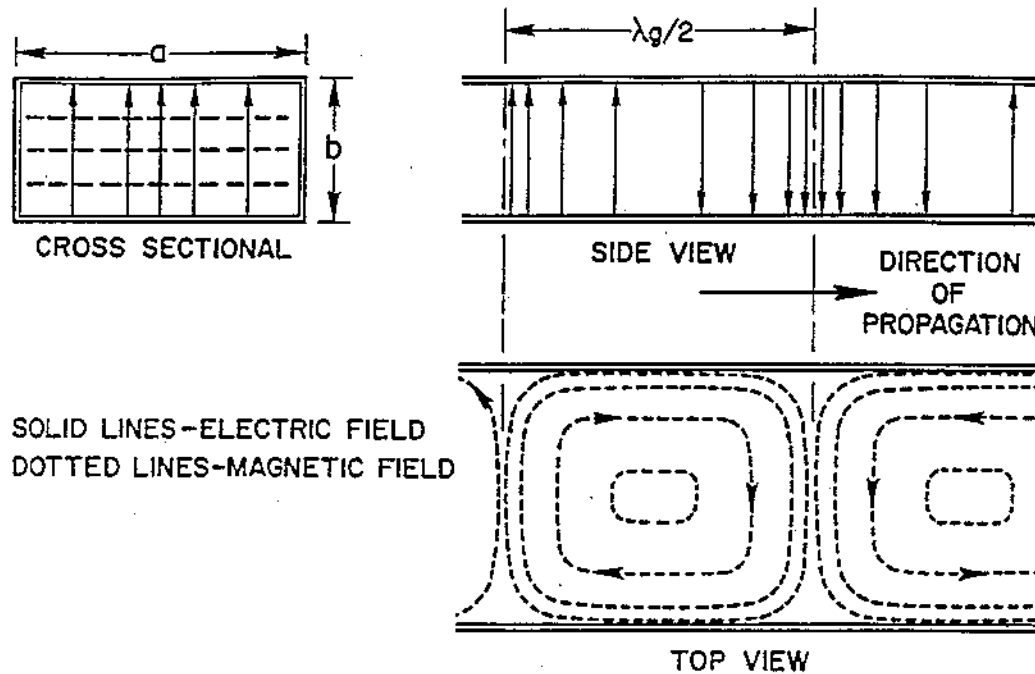


Microwave Measurements Laboratory

Components and Devices

Ralph J. Pasquinelli
Fermilab

Rectangular Wave Guide



Advantages: Low Loss, High Power

Disadvantages: Narrow bandwidth, bulky at low frequencies

$$\lambda_g = \frac{\lambda}{\sqrt{1 - \left(\frac{\lambda}{\lambda_c}\right)^2}}$$

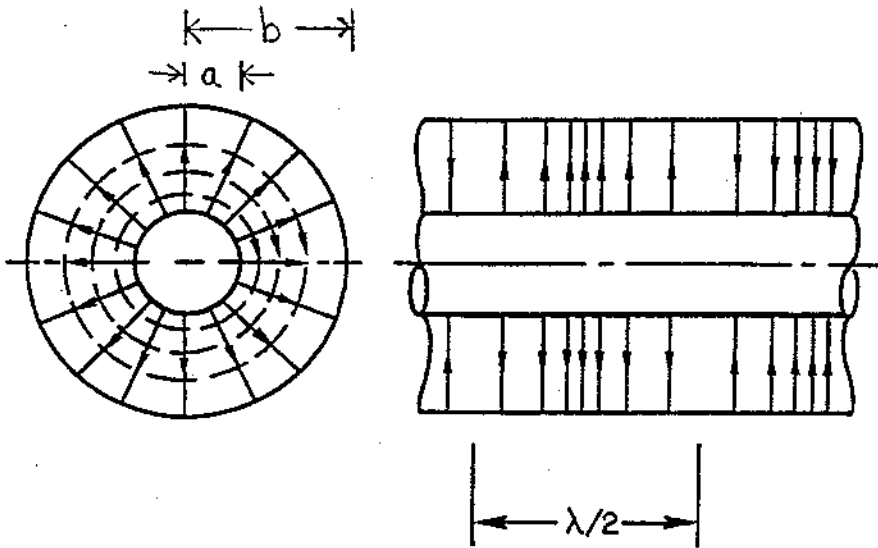
$$\lambda_{c_{TE10}} = 2a$$

Rectangular Wave Characteristics

EIA Waveguide Designation Standard (MIL-HDBK-216, S-261-A)	JAN Waveguide Designation (4 January 1962)	Outer Dimensions and Wall Thickness (in inches)	Frequency Range in Gigahertz for Dominant (TE _{1,0}) Mode	Cutoff Wave- length λ_c in Centimeters for TE _{1,0} Mode	Cutoff Frequency f_c in Gigahertz for TE _{1,0} Mode	Theoretical Attenuation, Lowest to Highest Frequency in dB/100 ft	Theoretical Power Rating in Megawatts for Lowest to Highest Frequency*
WR-2300	RG-290/U†	23.250×11.750×0.125	0.32-0.49	116.8	0.256	0.051-0.031	153.0-212.0
WR-2100	RG-291/U†	21.250×10.750×0.125	0.35-0.53	106.7	0.281	0.054-0.034	120.0-173.0
WR-1800	RG-201/U†	18.250×9.250×0.125	0.425-0.620	91.4	0.328	0.056-0.038	93.4-131.9
WR-1500	RG-202/U†	15.250×7.750×0.125	0.49-0.740	76.3	0.393	0.069-0.050	67.6-93.3
WR-1150	RG-203/U†	11.750×6.000×0.125	0.64-0.96	58.4	0.514	0.128-0.075	35.0-53.8
WR-975#	RG-204/U†	10.000×5.125×0.125	0.75-1.12	49.6	0.605	0.137-0.095	27.0-38.5
WR-770	RG-205/U†	7.950×4.100×0.125	0.96-1.45	39.1	0.767	0.201-0.136	17.2-24.1
WR-650	RG-69/U	6.660×3.410×0.080	1.12-1.70	33.0	0.908	0.317-0.212	11.9-17.2
WR-510	—	5.260×2.710×0.080	1.45-2.20	25.9	1.16	—	—
WR-430	RG-104/U	4.460×2.310×0.080	1.70-2.60	21.8	1.375	0.588-0.385	5.2-7.5
WR-340	RG-112/U	3.560×1.860×0.080	2.20-3.30	17.3	1.735	0.877-0.572	—
WR-284	RG-48/U	3.000×1.500×0.080	2.60-3.95	14.2	2.08	1.102-0.752	2.2-3.2
WR-229	—	2.418×1.273×0.064	3.30-4.90	11.6	2.59	—	—
WR-187	RG-49/U	2.000×1.000×0.064	3.95-5.85	9.50	3.16	2.08-1.44	1.4-2.0
WR-159	—	1.718×0.923×0.064	4.90-7.05	8.09	3.71	—	—
WR-137	RG-50/U	1.500×0.750×0.064	5.85-8.20	6.98	4.29	2.87-2.30	0.56-0.71
WR-112	RG-51/U	1.250×0.625×0.064	7.05-10.00	5.70	5.26	4.12-3.21	0.35-0.46
WR-90	RG-52/U	1.000×0.500×0.050	8.20-12.40	4.57	6.56	6.45-4.48	0.20-0.29
WR-75	—	0.850×0.475×0.050	10.00-15.00	3.81	7.88	—	—
WR-62	RG-91/U	0.702×0.391×0.040	12.40-18.00	3.16	9.49	9.51-8.31	0.12-0.16
WR-51	—	0.590×0.335×0.040	15.00-22.00	2.59	11.6	—	—
WR-42	RG-53/U	0.500×0.250×0.040	18.00-26.50	2.13	14.1	20.7-14.8	0.043-0.058
WR-34	—	0.420×0.250×0.040	22.00-33.00	1.73	17.3	—	—
WR-28	RG-96/U†	0.360×0.220×0.040	26.50-40.00	1.42	21.1	21.9-15.0	0.022-0.031

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Coaxial Transmission Lines



Advantages:

High Bandwidth, Small size

Disadvantages:

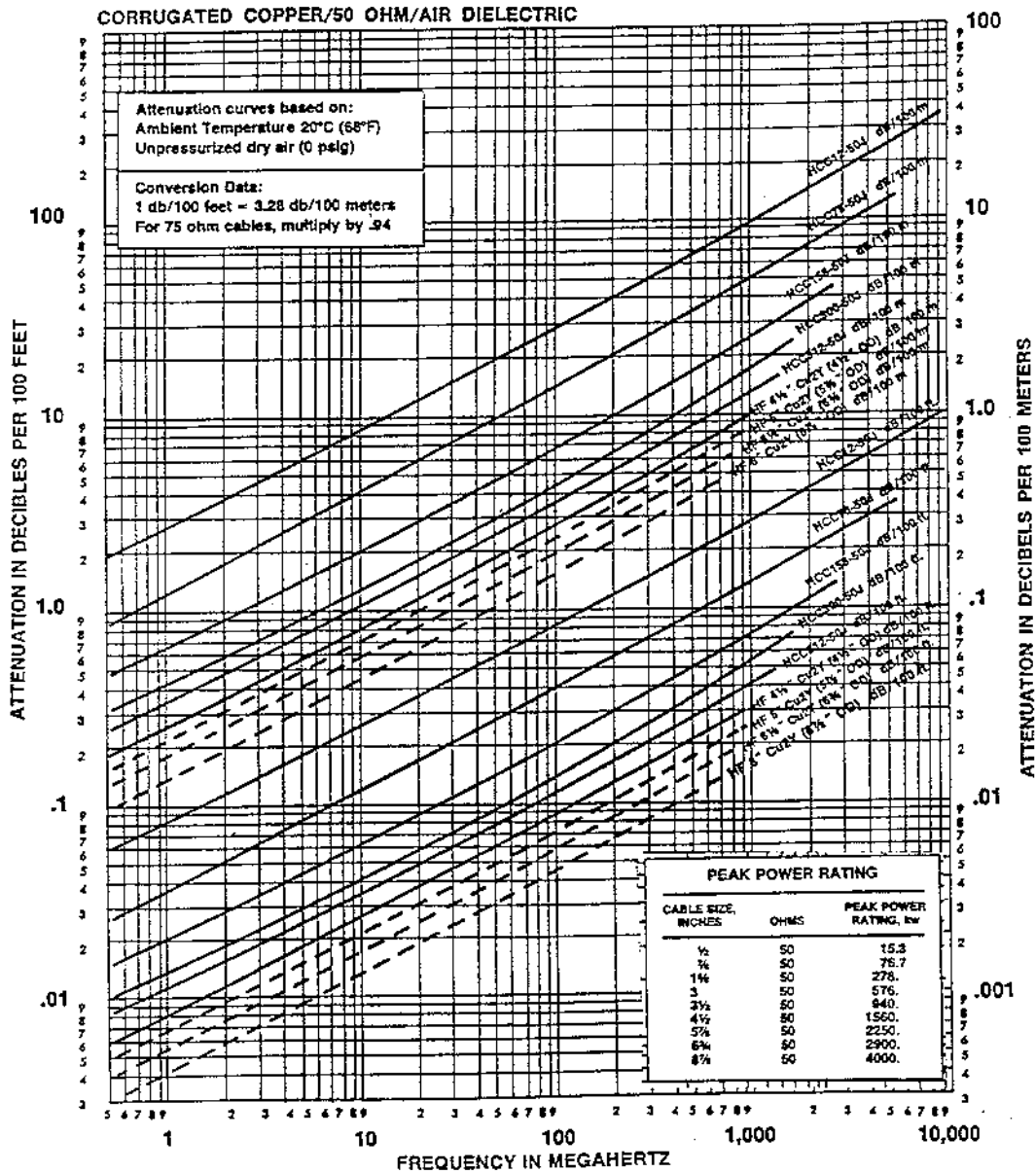
High loss, low power

$$Z_o = 60 \sqrt{\frac{\mu_r}{\epsilon_r}} \ln \frac{b}{a} \Omega$$

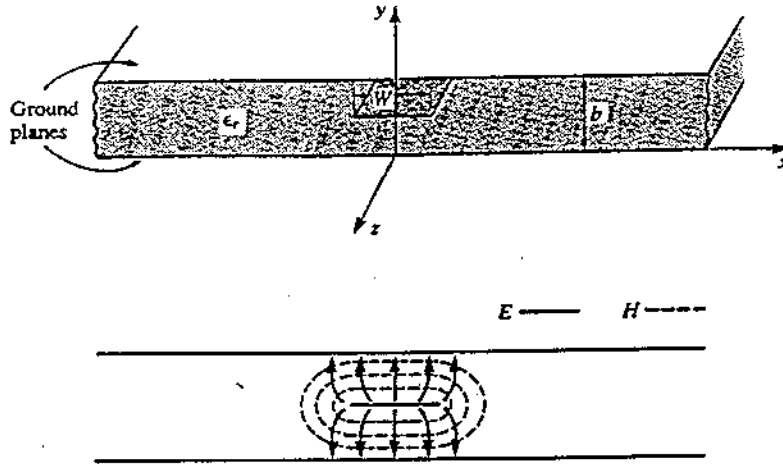
Coax Characteristics

Attenuation

Air Flexwell Cable

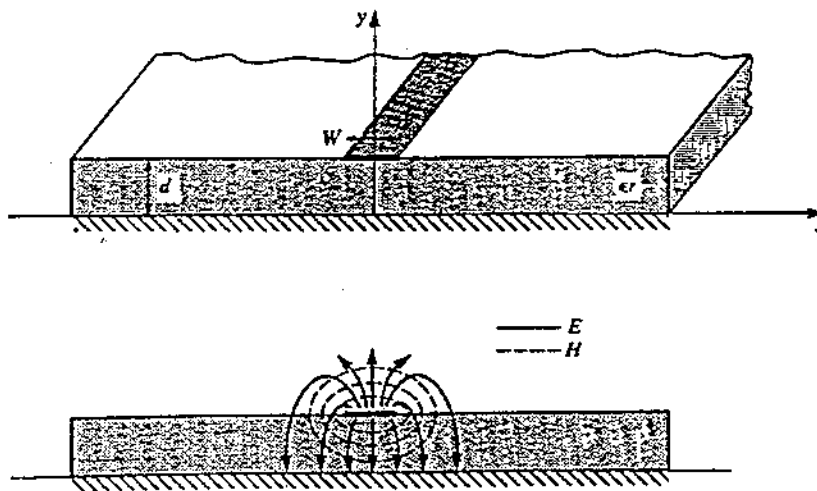


Stripline



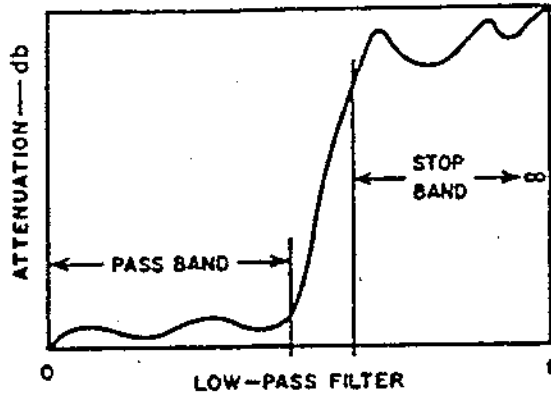
USED FOR
HYBRIDS
COUPLERS
FILTERS

Microstrip

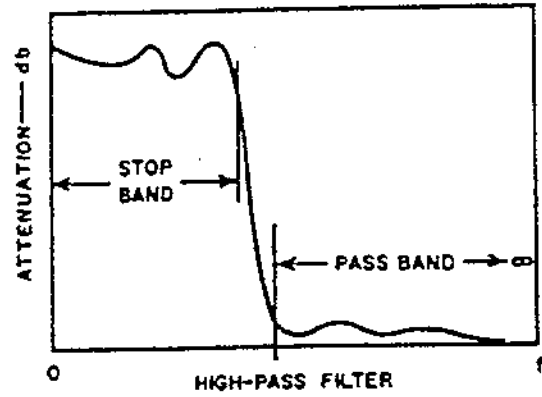


USED FOR
AMPLIFIERS
MIXERS
FILTERS

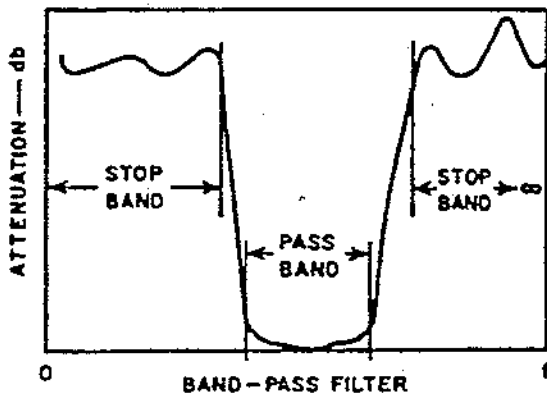
Filters



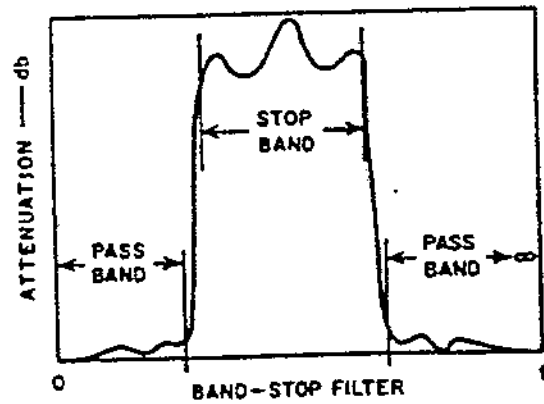
Lowpass



Highpass

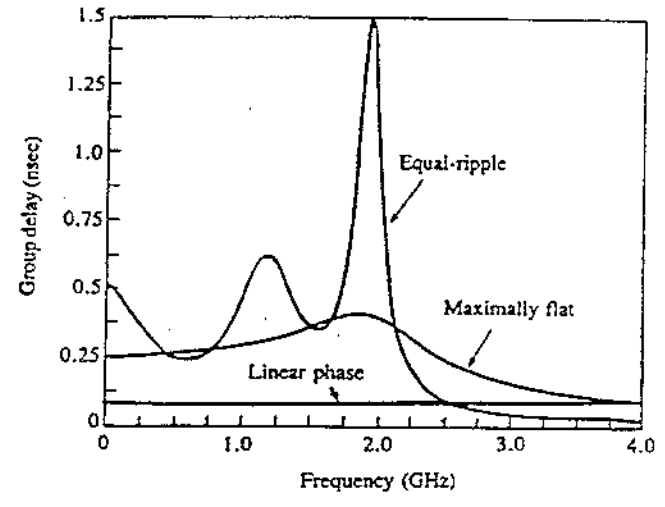
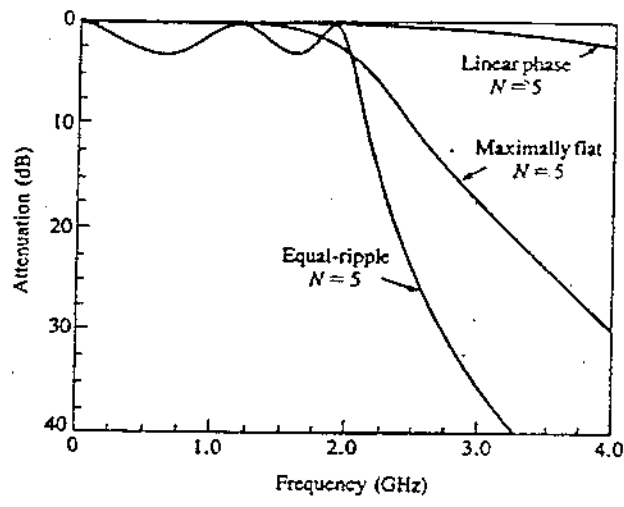


Bandpass

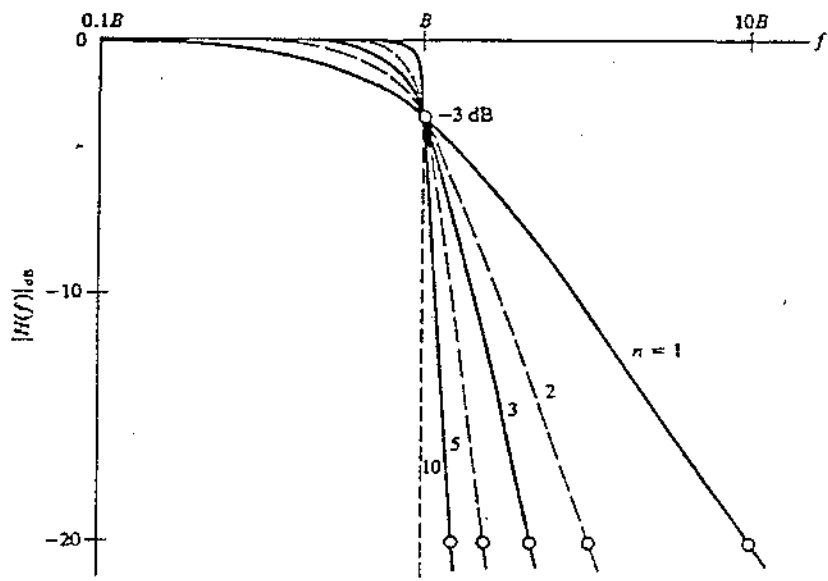


Bandstop

Filters Transfer Functions

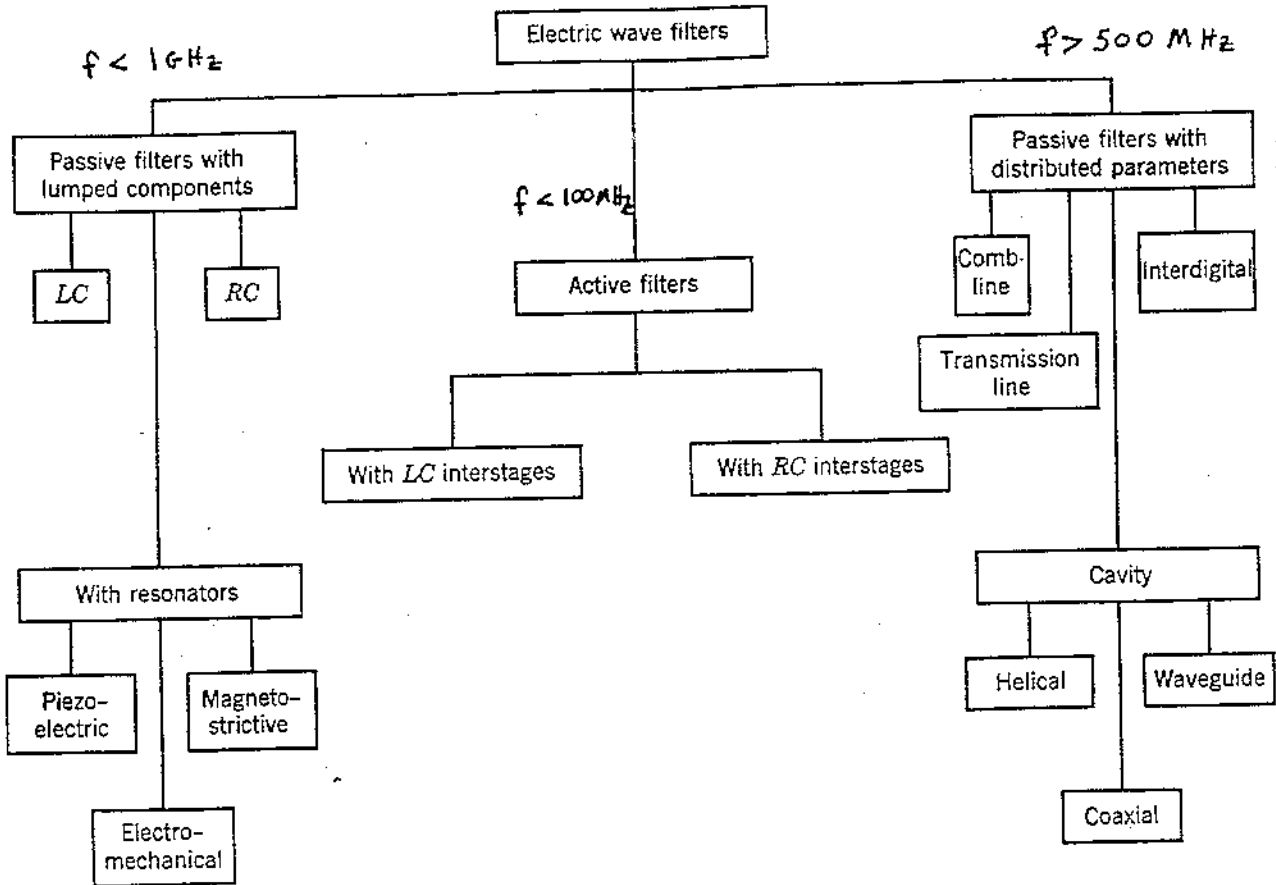


Transfer function for Butterworth lowpass filters of order n:

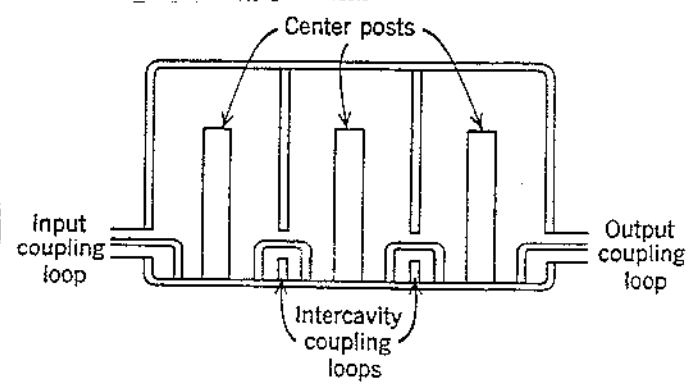
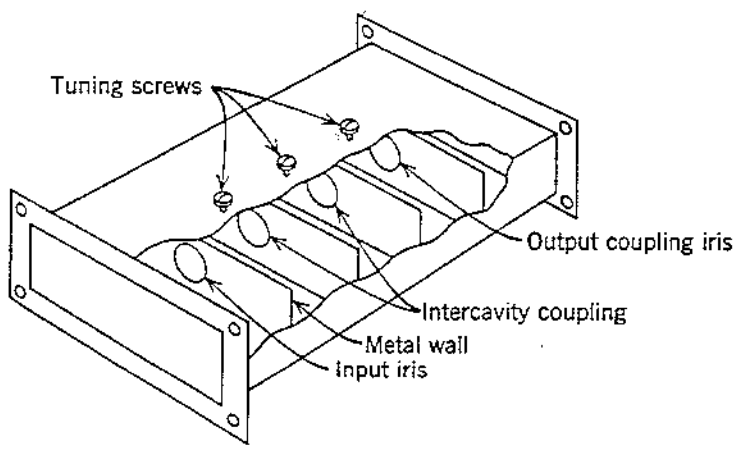
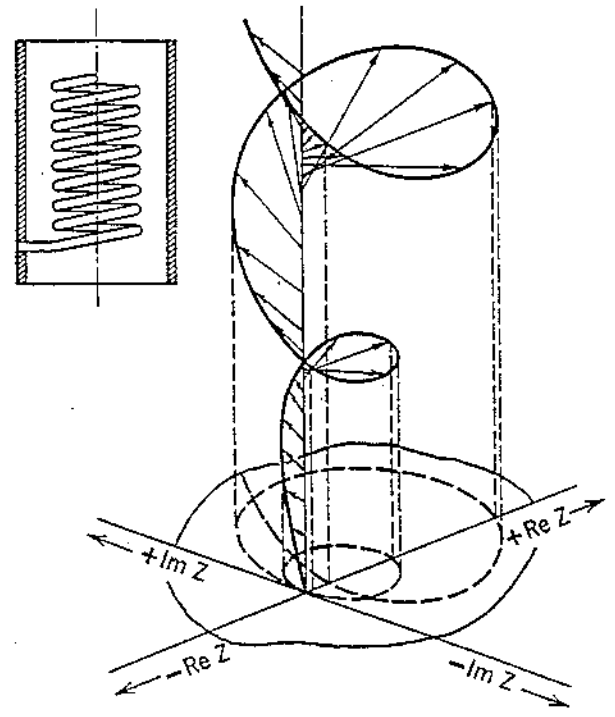
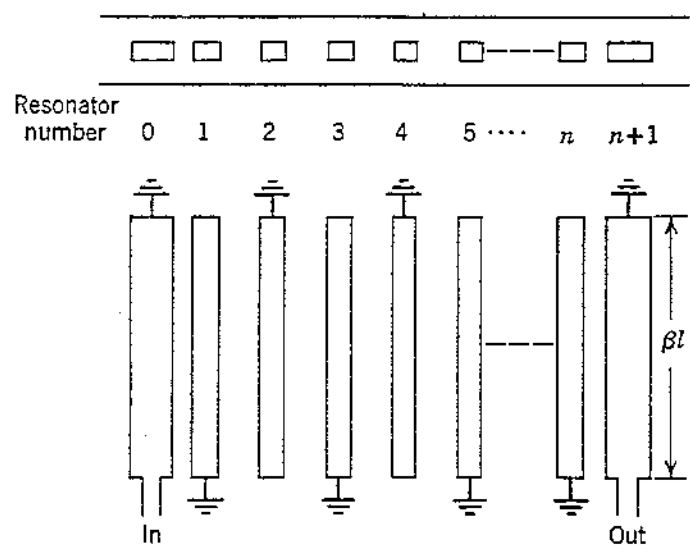
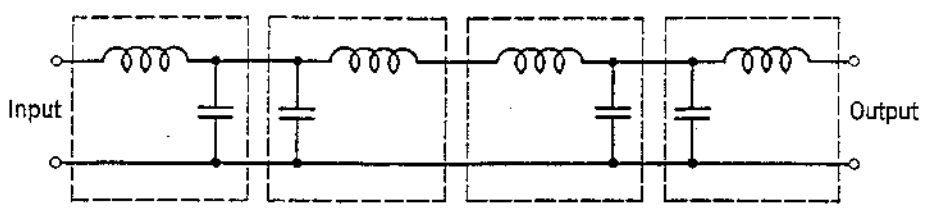
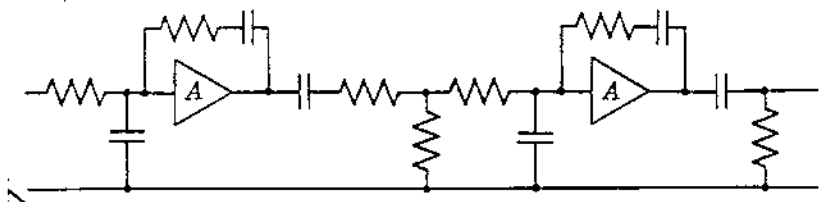


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Filter Classifications

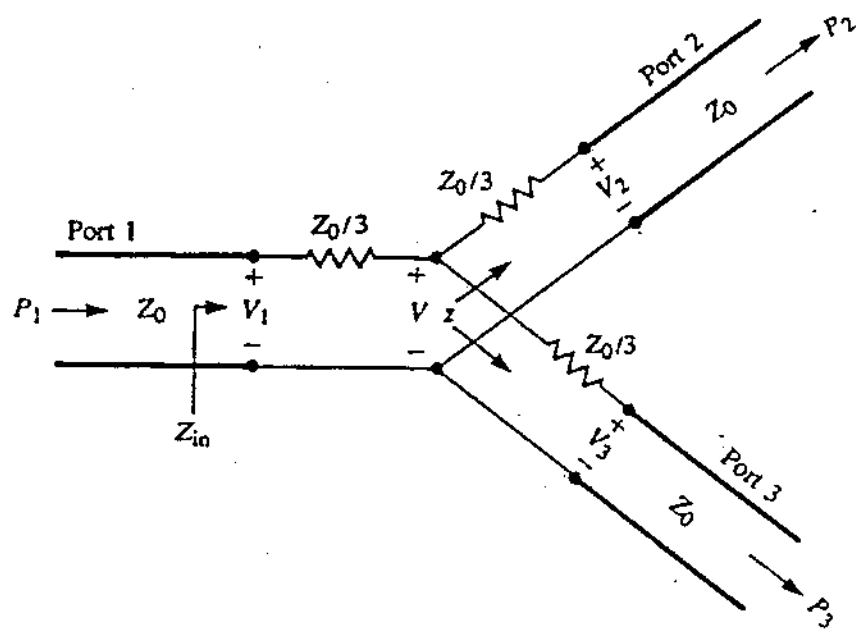


Filter Topologies



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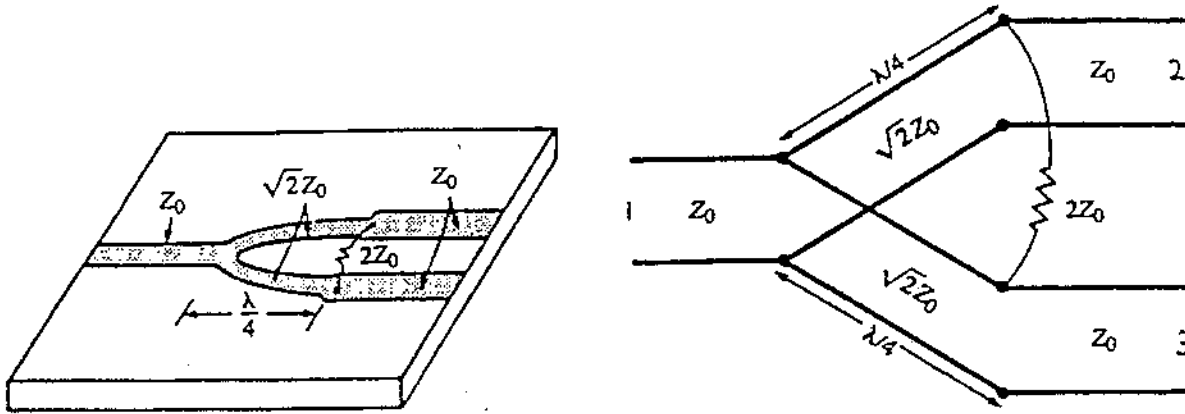
Resistive Power Splitter/Combiner



Advantages:
Disadvantages:

Multi Octave Broad Band
High Loss, low isolation

Wilkinson Power Splitter/Combiner

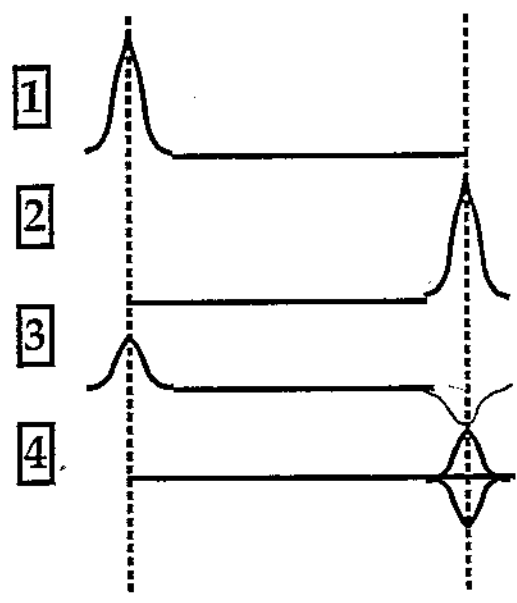
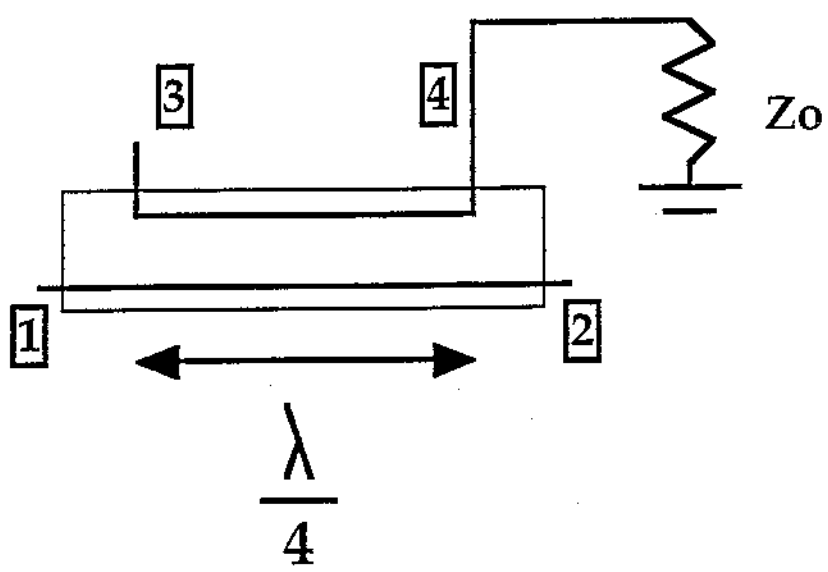


$$S \text{ parameters} = \begin{bmatrix} 0 & \frac{-j}{\sqrt{2}} & \frac{-j}{\sqrt{2}} \\ \frac{-j}{\sqrt{2}} & 0 & 0 \\ \frac{-j}{\sqrt{2}} & 0 & 0 \end{bmatrix}$$

Advantages: All ports matched and isolated,
low insertion loss

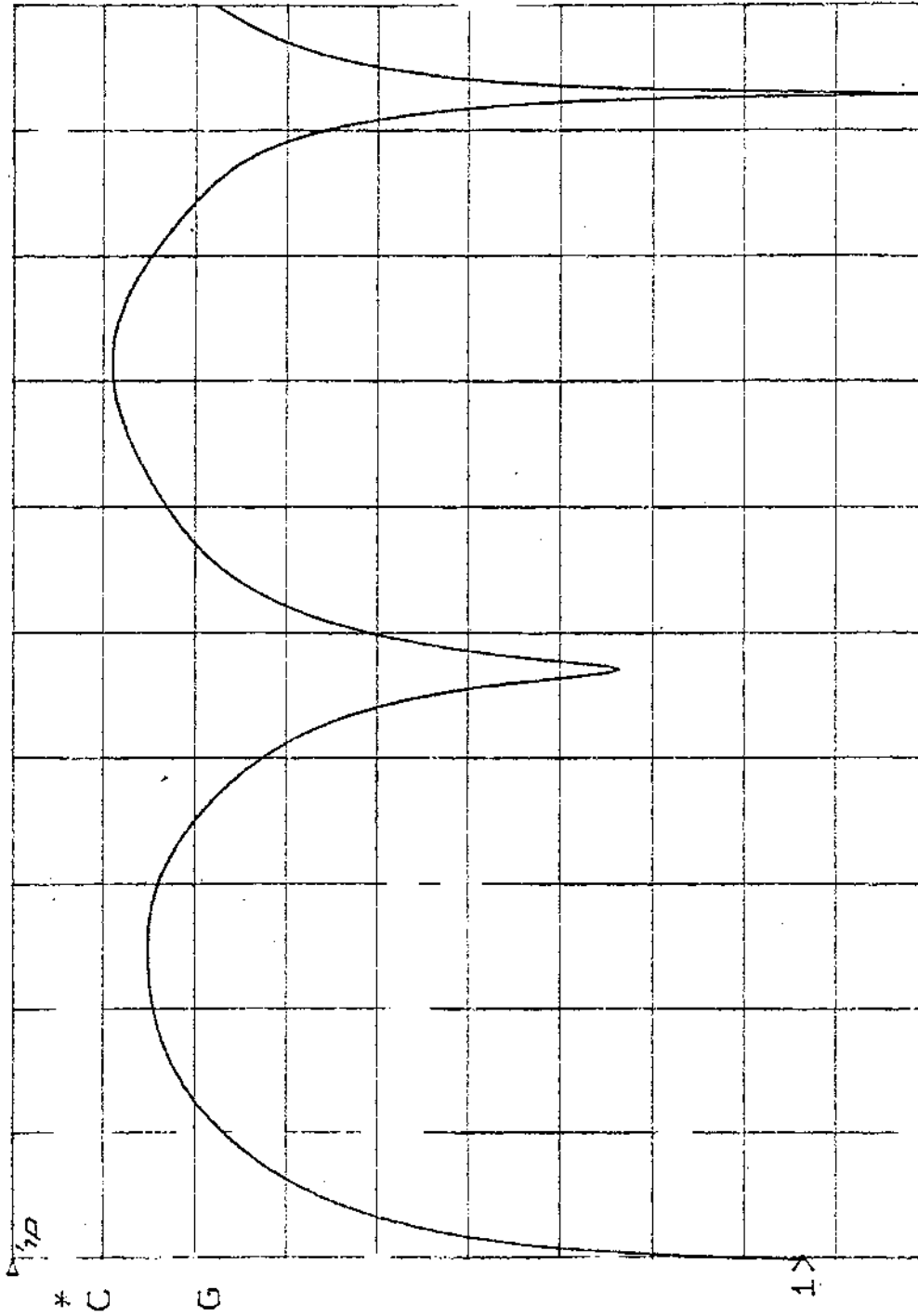
Disadvantages: Octave bandwidths typical

Directional Coupler



DIRECTIONAL COUPLER
FREQUENCY DOMAIN RESPONSE

► S21
REF -20.0 dB
5.0 dB



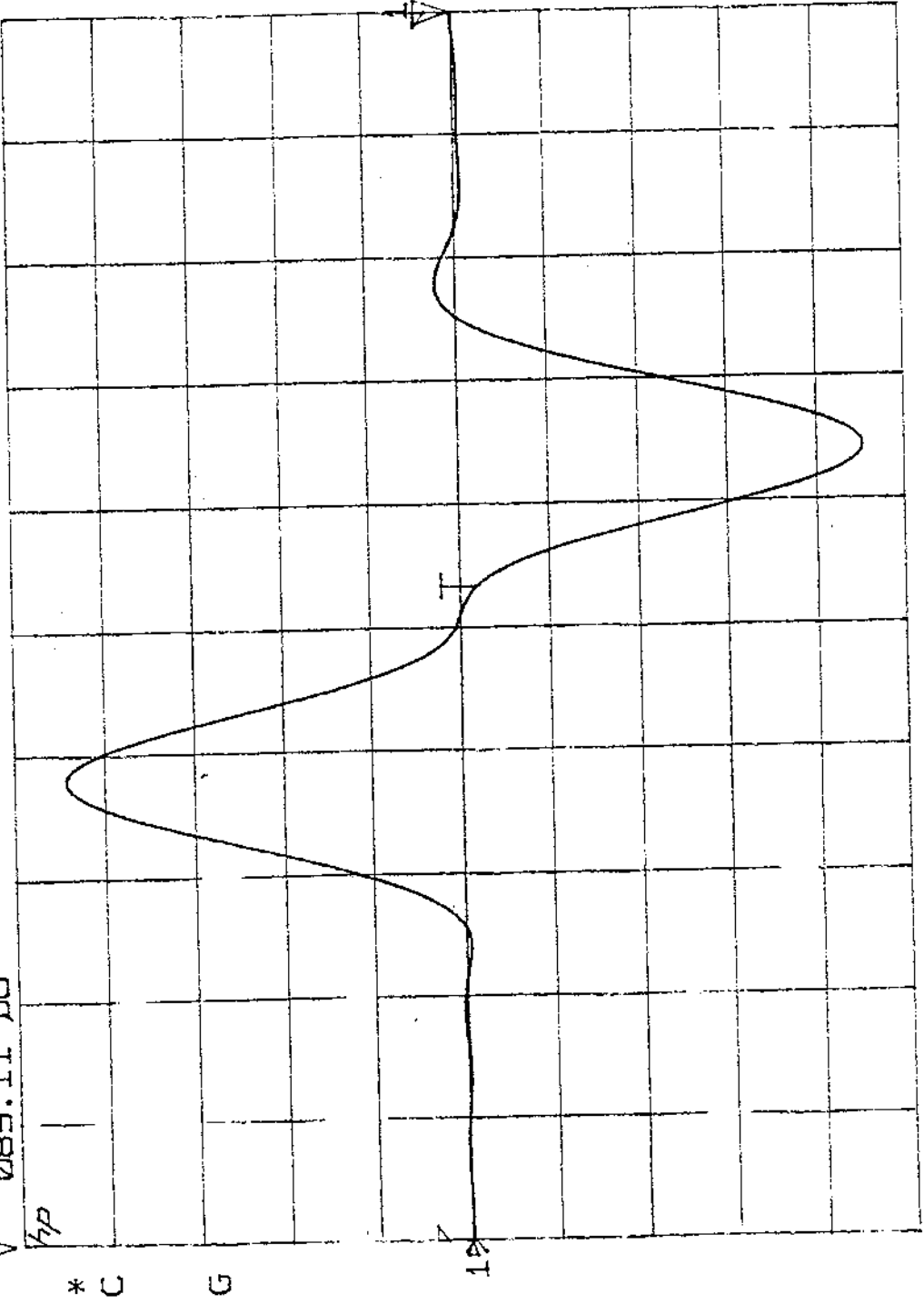
STAR 0.05000000 GHz
STOP 20.05000000 GHz

21 OCT 98
16:10:05

MARKER 1
 900.0 ps
 089.11 μ u

RE DIRECTIONAL COUPLER
 Time Domain RESPONSE

S21
 REF 0.0 Units
 1 5.0 mUnits
 089.11 μ u



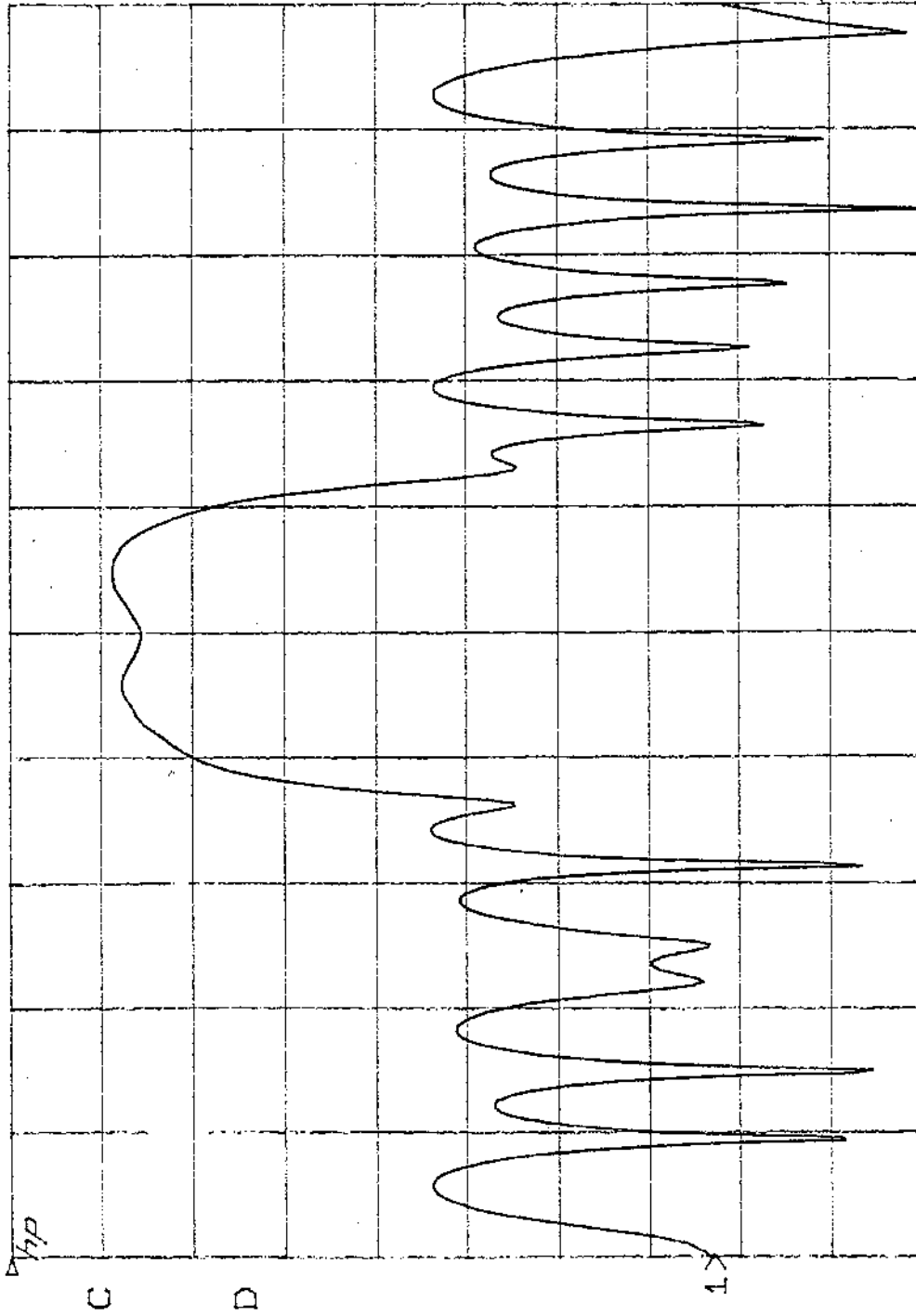
21 OCT 98
 16:13:53

START 500.0 ps
 STOP 900.0 ps

TRANSVERSAL FILTER

log MAG

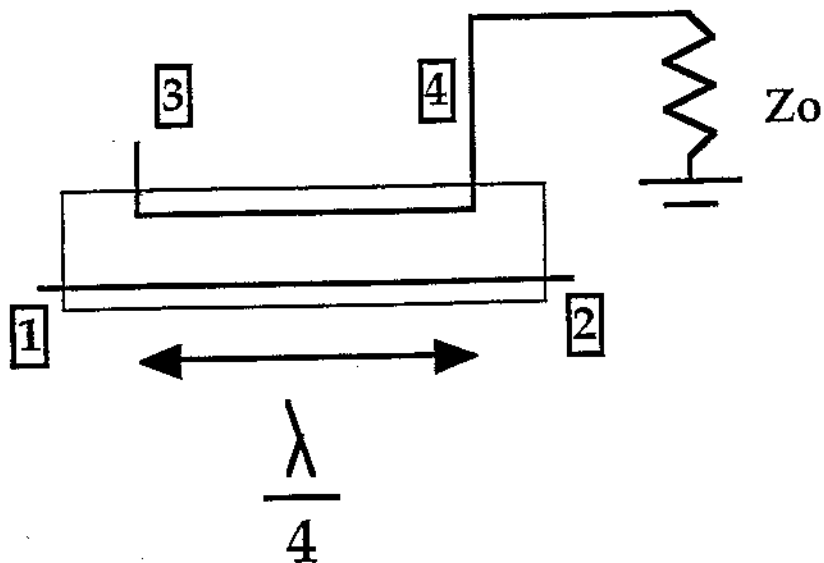
1521
REF 0.0 dB
5.0 dB



22 OCT 98
16:44:11

CENTER 4.250000000 GHz
SPAN 2.000000000 GHz

Directional Coupler Characteristics



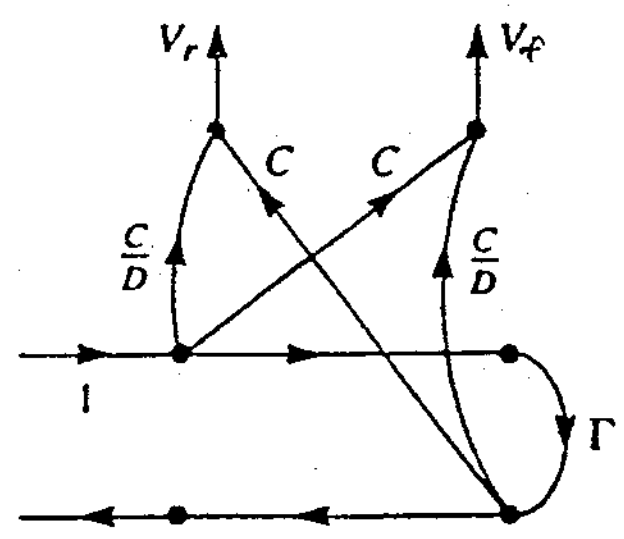
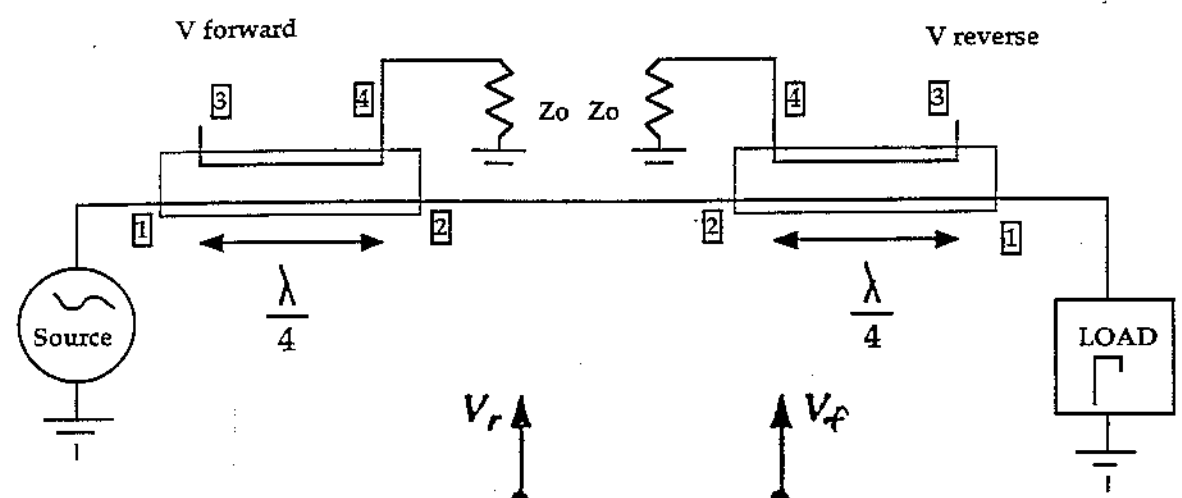
$$\text{Coupling Factor} = 10 \log \frac{P_1}{P_3} \text{ dB}$$

$$\text{Directivity} = 10 \log \frac{P_3}{P_4} \text{ dB}$$

$$\text{Isolation} = 10 \log \frac{P_1}{P_4} \text{ dB}$$

$$\text{Isolation} = \text{Directivity} + \text{Coupling factor}$$

Reflectometer



$$V_f = C \left[1 + \frac{1}{D} \Gamma e^{j\theta} \right]$$

$$V_r = C \left[\Gamma e^{j\theta} + \frac{1}{D} \right]$$

$$\left| \frac{V_r}{V_f} \right|_{\min}^{\max} = \frac{|\Gamma| \pm \frac{1}{D}}{1 \pm \frac{|\Gamma|}{D}}$$

90 Degree Hybrids

STRIPLINE CIRCUIT DESIGN

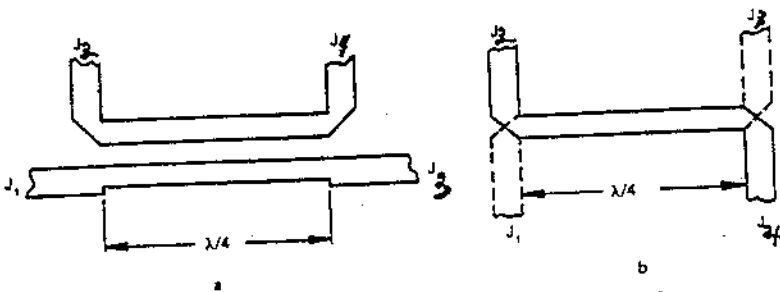


FIG. 5-1 Quarter-Wave Coupled-Line Directional Coupler Configurations

STRIPLINE CIRCUIT DESIGN

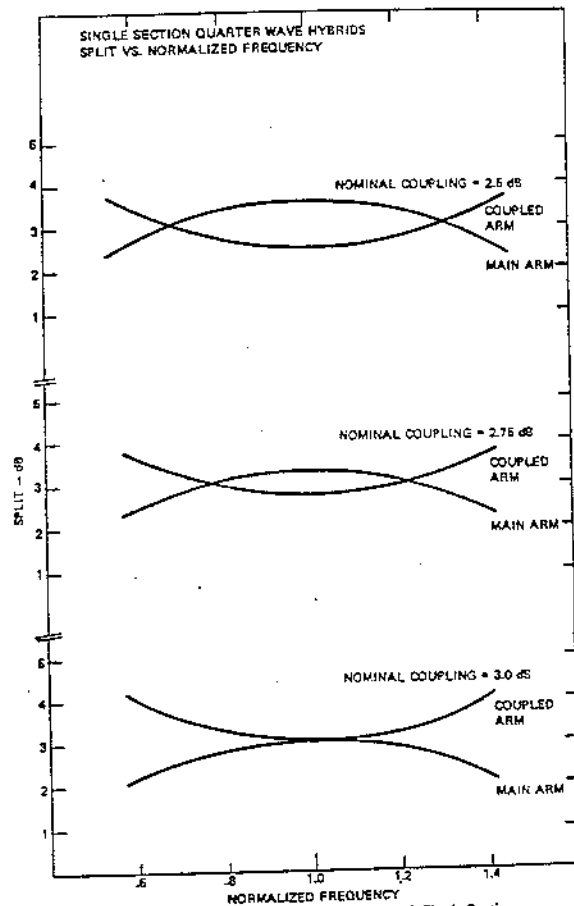
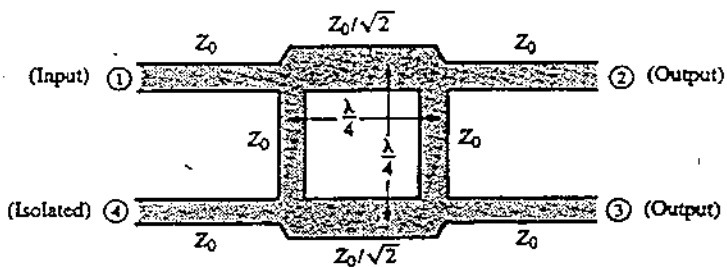


FIG. 5-5 Frequency Response for Several Single-Section Quarter-Wave 3.0 dB Hybrids for Varying Values of Nominal Coupling

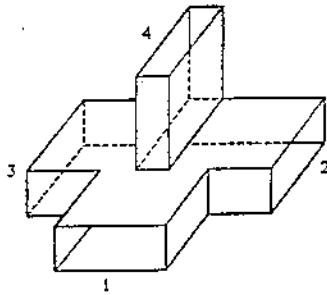
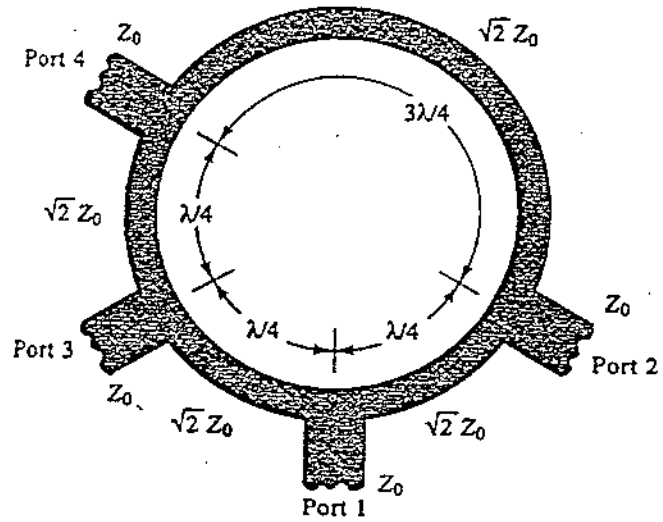


$$[S_{90}] = \frac{-1}{\sqrt{2}} \begin{bmatrix} 0 & j & 1 & 0 \\ j & 0 & 0 & 1 \\ 1 & 0 & 0 & j \\ 0 & 1 & j & 0 \end{bmatrix}$$

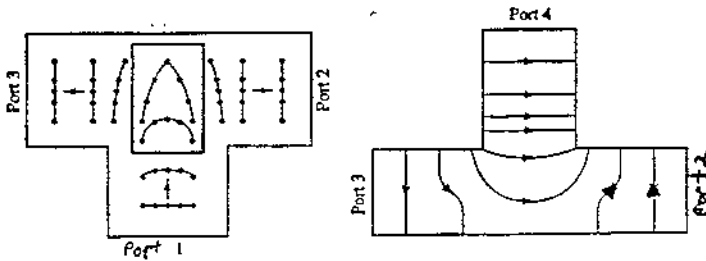
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180 Degree Hybrids

Ring Hybrid

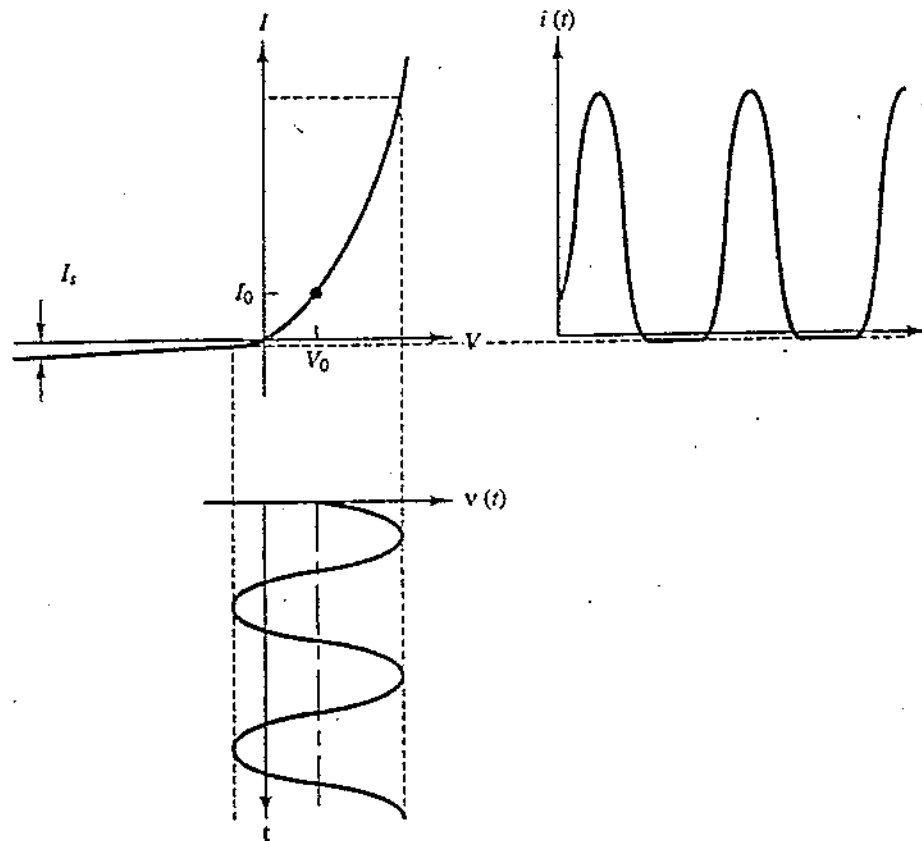


Waveguide Magic Tee



$$[S_{180}] = \frac{-j}{\sqrt{2}} \begin{bmatrix} 0 & 1 & 1 & 0 \\ 1 & 0 & 0 & -1 \\ 1 & 0 & 0 & 1 \\ 0 & -1 & 1 & 0 \end{bmatrix}$$

Diode Detectors



Square Law Detectors

$$i = a_0 + a_1 v + a_2 v^2 + a_3 v^3 + \dots$$

if

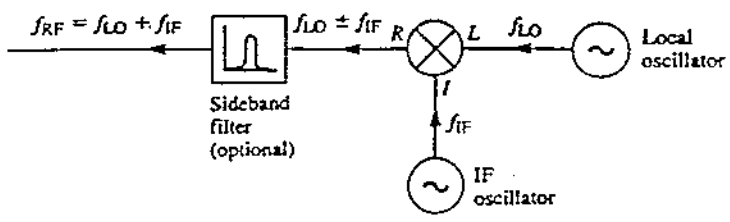
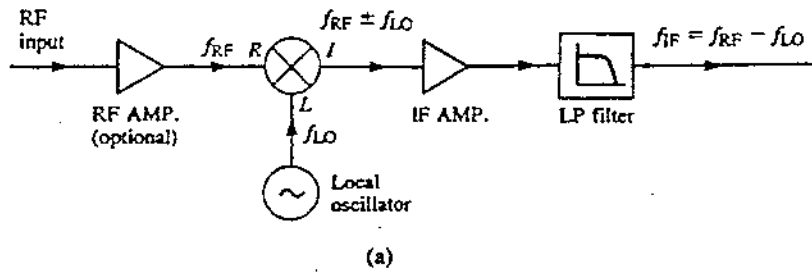
$$v = A \cos \omega t$$

$$i = a_1 (A \cos \omega t) + a_2 (A \cos \omega t)^2$$

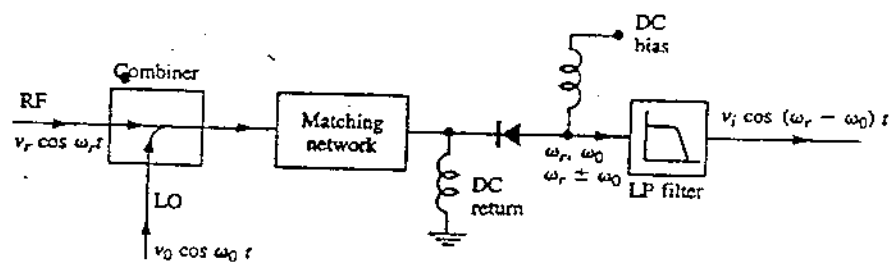
$$i = a_1 (A \cos \omega t) + \frac{a_2 A^2}{2} (1 + \cos 2\omega t)$$

Mixers

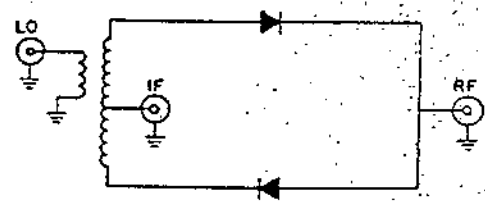
$$V_{out} = k V_{signal} V_{LO} [\cos(\omega_{LO} - \omega_{signal})t - \cos(\omega_{LO} + \omega_{signal})t]$$



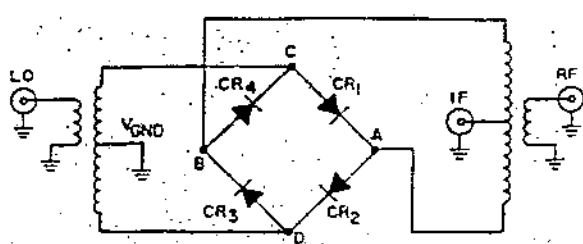
Single-ended
Simple design



Single Balanced
Improved input match
Isolation between RF and LO



Double Balanced
Improved Isolation between all ports
Suppresses even harmonics of RF and LO
Low conversion loss



References

- Microwave Theory and Applications, Stephen Adam , 1969
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- Microstrip Lines and Slotlines, Gupta, Garg, Bahl, 1979
- Cablewaves Systems, Catalog 600, 1986